

**UNITED STATES PATENT APPLICATION FOR:**

**POLARIZATION MITIGATION TECHNIQUE**

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**ATTORNEY DOCKET NUMBER: WEAT/0451**

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## **POLARIZATION MITIGATION TECHNIQUE**

### **BACKGROUND OF THE INVENTION**

#### **Field of the Invention**

[0001] This invention relates to measuring spectral responses of optical elements. More particularly, this invention relates to improving spectral response measurements by mitigating polarization dependence.

#### **Description of the Related Art**

[0002] Most optical components produce a spectral response that depends on the polarization of incident light. This is often manifested as a polarization-dependent shift in the wavelength of a spectral characteristic (e.g. a reflection peak wavelength) of an optical component. If the incident light is highly polarized, this polarization dependence can cause significant shifts in the wavelength of the spectral characteristic. In many systems, the polarization of the incident light is varying and unknown. This results in unpredictably varying shifts in the wavelengths of the spectral characteristic.

[0003] One of the many optical elements having polarization-dependent shifts in wavelength is the fiber Bragg grating (FBG) element. A fiber Bragg grating (FBG) element is an optical element that is usually formed by photo-induced periodic modulation of the refractive index of an optical fiber's core. An FBG element is highly reflective to light having wavelengths within a narrow bandwidth that is centered at a wavelength that is referred to as the Bragg wavelength. Other wavelengths are passed without reflection. The Bragg wavelength itself is dependent on physical parameters, such as temperature and strain, that impact on the refractive index. Therefore, FBG elements can be used as sensors to measure such parameters. After proper calibration, the Bragg wavelength is an absolute measure of the physical parameters.

[0004] FBG sensors typically include a tunable laser that interrogates an FBG element by sweeping across an optical spectrum that includes that Bragg wavelength. Alternatively, a broadband light source/tunable filter combination

can be used. The sweeping light generates reflections from the FBG element that produce a spectral response of intensity verses wavelength. Since the spectral response peaks correspond to the Bragg wavelengths of the FBG element, by determining the changes in response peaks produced by the physical parameter of interest that parameter can be measured.

[0005] Unfortunately, in FBG sensors, the polarization-dependent wavelength shift can limit the achievable measurement accuracy and resolution. This is because the spectral response peaks change not only because of the physical parameter of interest, but also because of polarization induced wavelength shifts.

[0006] That polarization-dependent wavelength shifts can impact measurements is known, see reference Vines, Lasse, "Polarization Dependence in CHERS Fiber Optic Strain Monitoring System Based on Fiber Bragg Gratings", Norwegian Defense Research Establishment doc #: FFI/RAPPORT-2002/03348, ISBN-82-464-0645-0. That reference describes attempts at mitigating the polarization problem by depolarizing the source radiation. However, when using narrow-bandwidth sources this puts stringent requirements on the depolarizer design, often beyond what is practically achievable.

[0007] Therefore, a new method and apparatus of compensating for polarization-dependent wavelength shifts would be beneficial.

### **SUMMARY OF THE INVENTION**

[0008] The principles of the present invention enable compensation of polarization-dependent wavelength shifts in optical filter elements.

[0009] A polarization mitigated measurement apparatus that is in accord with the present invention includes an optical source that scans across an optical spectrum. That optical source is applied to a polarization element that changes the polarization of the output light. The output of the polarization element is applied to an optical filter element that is subject to polarization-dependent

wavelength shifts. The bandwidth of the optical filter element is significantly greater than the rate of change of the polarization of the polarization element. The optical filter element produces a spectral response with an unknown polarization-induced wavelength-shift transformation. A spectral measurement network measures that spectral response and produces a received signal across the optical spectrum. A data processing unit then calculates a filter wavelength that is insensitive to the polarization-induced variations in the received signal across the bandwidth of the optical filter element. That calculated filter wavelength is subsequently used to characterize the optical filter element.

### **BRIEF DESCRIPTION OF THE DRAWINGS**

[0010] So that the manner in which the above recited features of the present invention can be understood in detail, a more particular description of the invention, briefly summarized above, may be had by reference to embodiments, some of which are illustrated in the appended drawings. It is to be noted, however, that the appended drawings illustrate only typical embodiments of this invention and are therefore not to be considered limiting of its scope, for the invention may admit to other equally effective embodiments.

[0011] Figure 1 schematically illustrates an optical system that incorporates the principles of the present invention;

[0012] Figure 2 illustrates both the spectral response and its dependence on polarization of an FBG sensor;

[0013] Figure 3 illustrates the use of a low-order (2nd) polynomial curve fit to produce a measurement insensitive to polarization-induced variations;

[0014] Figure 4 illustrates the spectral response of Figure 2 both before and after that response is filtered; and

[0015] Figure 5 schematically illustrates an FBG sensor system that incorporates the principles of the present invention;

[0016] To facilitate understanding, identical reference numerals have been used, wherever possible, to designate identical elements that are common to the figures.

## **DETAILED DESCRIPTION OF ILLUSTRATED EMBODIMENTS**

[0017] Referring now to Figure 1, a polarization mitigated apparatus 20 that is in accord with the present invention includes an optical source 24 that scans across an optical spectrum. The optical source 24 is coupled to a polarization changing device 28 that changes the polarization of the optical radiation (light) in a particular manner that is described subsequently. The output of the polarization changing device 28 is applied to an optical element 32 that produces an unknown and/or varying polarization transformation on the optical radiation. The optical radiation (light) is then applied to an optical element 72 having a polarization dependent wavelength response. The response of element 72 has some spectral feature, or spectral features, of interest within the optical spectrum produced by the optical source 24. The optical elements 32 and 72 may also comprise a single element having the same functionality as described above.

[0018] The bandwidth of the optical feature of interest in the optical element 72 is significantly greater than the rate of change of the polarization of the polarization changing device 28. That is, the polarization changing device 28 changing polarity slowly: Such a slow change corresponds to a narrow bandwidth.

[0019] Figure 2 is an exemplary diagram 36 of the spectral response of the optical element 72 to light from the system described above. The polarization dependency of the optical element 72 results in a spectral waveform 40 of wavelength (in the X-axis 44) against normalized amplitude (in the Y-axis 48). Curves 52 and 60 represent the spectral response of the feature of interest of element 72 for incident radiation on each of two orthogonal polarization axes. Waveform 40 represents the response of the feature of interest (Bragg wavelength) as a mixing of the two orthogonal polarization responses 52 and 60

due to the polarization changing device 28. The diagram 36 might be a plot of transmission through the optical element 72 or reflections from the optical element 72.

[0020] In any event, the light from the optical element 72 is detected and converted into electrical signals-by a receiver 64. The output of the receiver 64 is applied through an optional low pass filter 68 (whose purpose is described subsequently) to a data processor 76 that derives a parameter of interest, e.g., a Bragg wavelength, from the receiver output. A further, alternative arrangement is for a low pass filter to be an integral part of the receiver 64.

[0021] The receiver 64 produces electrical signals that correspond to the spectral waveform 40. Thus, the waveform 40 also represents electrical signals. In some embodiments of the present invention the data processor 76 uses a noise insensitive peak detection method to characterize the wavelength of the spectral feature 40. Wherein such noise may be randomly produced or produced from a systematic source. An example of such a technique is shown in figure 3 wherein the spectral feature 40A is being characterized. As shown, a quadratic curve 80 has been fit to the measured signal 40A with a least-square error minimization technique. Examples of other suitable peak detection schemes include: center of mass/centroid calculations, a fit of a polynomial curve, a Gaussian curve, a Lorentzian curve, various power sine/cosine or other trigonometric function curves, etc. Other curve fit methods may also be used. Regardless of the specific method used, in certain embodiments it is advantageous that the calculation of the wavelength corresponding to the spectral feature is insensitive noise or variation at a frequency greater than the bandwidth of the spectral feature of interest.

[0022] Another approach to improving peak detection is to incorporate the optional low-pass filter 68. That low-pass filter should have a cut-off frequency that filters the higher frequency ripple content from the electrical signal 40. This is shown, in Figure 4, wherein the electrical waveform 40A is smoothed by filtering to produce the waveform 90, which has reduced peaks and valleys.

This filtering could be analogue or digital, finite impulse response or infinite impulse response, or any combination of these.

[0023] It should be understood that a low pass filter, noise insensitive peak detection techniques, or both can be used. Thus, low pass filtering and noise insensitive peak detection techniques are complementary rather than mutually exclusive.

[0024] Turning back to Figure 1, the optical source 24 could be any of a number of devices such as a tunable laser or a combination of a broadband light source and a tunable filter. The polarization changing device 28 can be a depolarizer or a polarization scrambler, either active or passive. It could also be integrated into the source 24, or even be an inherent property of the source 24. Commonly used passive depolarizers include wedge depolarizers, cascaded feed-back loop depolarizers and Lyot depolarizers. Commonly used polarization scramblers include Lithium Niobate, resonant coil or fiber squeezer based devices.

[0025] The optical element 32 that produces the unknown polarization transformation can be any of a wide range of optical elements. Indeed, most optical elements show polarization dependence in their transmission or reflection spectral responses. An example of such an optical element is the fiber optic cable. Not only do fiber optic cables show polarization dependence, but fiber optic cables can incorporate fiber Bragg grating elements that also exhibit polarization dependence. As previously noted, fiber Bragg grating elements can be used in FBG sensor systems.

[0026] Figure 5 illustrates a specific embodiment of the invention, specifically an FBG sensor system 118 having FBG elements 120 within an FBG sensor array 130. As shown, the FBG sensor array 130 may be comprised of one or more optical fibers 145 and 147. The individual FBG elements 120 have Bragg wavelengths  $\lambda_1$  through  $\lambda_5$ . As noted, Bragg wavelengths are dependent upon physical parameters such as temperature and pressure, and thus changes in wavelengths  $\lambda_1$ - $\lambda_5$  can be made indicative of parameters being sensed.

Unfortunately, measurement errors caused by polarization shifts in the optical fibers and other optical elements can reduce the accuracy.

[0027] The FBG sensor system 118 is suitable for measuring pressure and temperature in hostile environments such as occurs in oil wells. To provide a reference wavelength the FBG sensor system 118 includes an optical fiber 149 having a reference FBG element 160 that is physically and thermally protected by an enclosure 162. The reference FBG element 160 is comprised of a fiber Bragg grating 166 that is induced in the core of the optical fiber 149. When light is applied to the reference FBG element 160 reflections of light at Bragg wavelengths are produced. The enclosure 162 protects the reference FBG element 160 such that its Bragg wavelengths are not susceptible to external influences and thus are accurately known. Alternatively, a thermometer could be used to determine the temperature of the reference FBG element 160. Then, based on the measured temperature the Bragg wavelengths of the FBG element 160 could be temperature compensated. Either way, the reference FBG element 160 produces Bragg wavelengths that are accurately known and that can be used to process other Bragg wavelengths. Any measurement error in the Bragg wavelength of the reference FBG element 160 caused by polarization shifts in the optical fiber 149 or in other optical elements will reduce the accuracy of all of the Bragg wavelength measurements.

[0028] The FBG sensor system 118 further includes a tuned laser 140 that is scanned across the Bragg wavelengths of the FBG elements 120 and of the reference FBG element 160. The tuned laser 140 corresponds to the source 24 of Figure 1. The narrow bandwidth scanning light is applied to a polarization changing device 28 (also see Figure 1 and the foregoing description of the polarization changing device 28), which generically represents polarization changes induced by the tuned laser 140 and by the optical transmission path. Other optical elements, including the optical fibers 145, 147, and 149, can also induce polarization changes.

[0029] The output of the polarization changing device 28 is split by a fiber optic directional coupler 180. The main portion of that light is coupled to the FBG



sensor array 130 and to the reference FBG element 160 via a second directional coupler 202. Reflected light from the FBG sensor array 130 and from the FBG element 160, which occur when the wavelength of the narrow bandwidth scanning light sweeps across the Bragg wavelength of an FBG element 120 or of the reference FBG element 160, passes back into the directional coupler 202 and into a sensor receiver network 219. That receiver includes a sensor detector 220 that converts the Bragg wavelength reflections into sensor electrical signals having amplitudes that depend on the power (intensity) of the reflected light. Thus, the sensor detector 220 acts as a power meter.

[0030] The output of the sensor detector 220 is applied to a sensor electrical filter 226 (which corresponds to the filter 68 of Figure 1), which is part of the sensor receiver 219. The sensor electrical filter 226 low-pass filters the sensor electrical signals to reduce the polarization dependent portions of the electrical signals. The polarization dependent portions can be caused by polarization changes induced by the polarization changing device 28 and by the optical fibers 145, 147, or 149.

[0031] The output of the sensor electrical filter 226 is applied to a sensor amplifier 228, which is also part of the sensor receiver 219. The sensor amplifier 228 amplifies the output of the sensor electrical filter 226. Alternatively, the sensor amplifier 228 could come before the sensor electrical filter 226, or sensor electrical filters 226 can be placed both before and after the sensor amplifier 228.

[0032] A portion of the light from the fiber optic directional coupler 180 is directed along a reference arm 250 having an interference filter 326, which is, for example, a fixed cavity F-P fiber filter. The interference filter 326 produces a reference spectrum having spectrum peaks with a constant, known frequency separation that depends on the interference filter 326. The reference spectrum is coupled to a reference receiver 329. The reference receiver 329 includes a reference detector 330 that produces a reference electrical pulse train that corresponds to the output of the interference filter 326. The output of the

reference detector 330 is filtered by a reference filter 332, which is part of the reference receiver 329. The reference filter 332 low pass filters the reference electrical signals to reduce the polarization dependent portions of the electrical signals. The output of the reference filter 332 is applied to a reference amplifier 336, which is also part of the reference receiver 329, and which amplifies the output of the reference filter 332. Alternatively, the reference amplifier 336 could come before the reference filter 332.

[0033] Once the wavelength of one of the reference spectrum peaks is known, because of the constant frequency separation produced by the interference filter 326 all of the wavelengths of the peaks can be determined. Then, by comparing the Bragg wavelengths of the FBG elements 120 to the wavelengths of the reference spectrum peaks the Bragg wavelengths of the FBG elements can be accurately determined. Furthermore, since the unstressed Bragg wavelengths of the FBG elements 120 are known, the wavelength change in each FBG element's Bragg wavelength can be used to determine a physical parameter of interest.

[0034] To that end, the electrical signals from the sensor receiver 219 and from the reference receiver 329 are sequentially sampled, processed and compared in a signal processing and data presentation unit 366 to produce such measurements. That unit interrogates the reference electrical signals to isolate the responses from the reference FBG element 160 (which are different than the wavelengths  $\lambda_1$  through  $\lambda_5$ ). Those responses are then processed as is described below to produce a characteristic wavelength of the reference FBG element 160. That characteristic wavelength is then used to identify at least one reference peak, which together with the known reference peak spacing, are used as to determine the Bragg wavelengths  $\lambda_1$  through  $\lambda_5$ .

[0035] A key to accurately determining Bragg wavelengths  $\lambda_1$  through  $\lambda_5$  is accurately determining the characteristic Bragg wavelength of the reference FBG element 160. To determine that Bragg wavelength the signal processing and data presentation unit 366 performs a mathematical analysis of the reference electrical signals and of the sensor electrical signals to reduce

polarization induced measurement errors. That analysis uses signal processing techniques that are insensitive to and/or that remove unwanted noise and fluctuations in the received signals from both the reference receiver 329 and from the sensor receiver 219. The analysis can include mathematical techniques such as fitting quadratic curves to the electrical signals using a least-square error minimization technique as described above. Of course, other mathematical techniques could be used. Furthermore, the low-pass filtering of the reference electrical signals and of the sensor electrical signals also reduce polarization induced measurement errors. By compensating for polarization induced changes the measurement accuracy can be improved.

[0036] While the foregoing is directed to embodiments of the present invention, other and further embodiments of the invention may be devised without departing from the basic scope thereof, and the scope thereof is determined by the claims that follow.